

Bimanual Haptic Telepresent Control and its Application to Deactivation of Mines: *Concepts, Implementation, and Evaluation*

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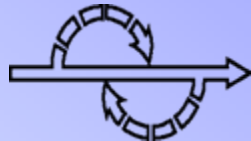
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Abstract

This presentation discusses a novel approach to support disposal of explosive ordnances by application of bimanual haptic telepresent control techniques. For improved task execution the proposed system enables a human operator to perceive multimodal feedback, in particular detailed kinesthetic and tactile feedback at arms and fingers, from a remote task environment. Details of the developed experimental setup, comprising stereo vision, an active two-handed human system interface and a corresponding two-arm teleoperator, are presented. Furthermore a novel structure adapting scheme for control of the force feedback display and the manipulator arms is introduced. Usability and effectiveness of the bimanual telepresent control system are demonstrated by focusing and evaluating as a most relevant task scenario, the execution of mine defusing operations in a remote task environment.



Related Publications

Schmidt, G.; Kron, A.:

Haptic Telepresent Control Technology Applied to Disposal of Explosive Ordnances: Principles and Experimental Results. Proc. of the IEEE Int. Symposium on Industrial Electronics, *ISIE'05* Dubrovnik, Croatia, pp. 1503-1510.

Kron, A.; Schmidt, G.:

Stability and Performance Analysis of Kinesthetic Control Architectures for Bimanual Telepresence Systems.

J. of Intelligent and Robot Systems (2006) 46,
Springer Science +Business Media B.V., pp. 1 -26.

Baier, H.; Schmidt, G.:

Transparency and Stability of Bilateral Kinesthetic Teleoperation with Time- Delayed Communication.

J. of Intelligent and Robot Systems (2004) 40:, 1-22, p. 1-12.



Background: Disposal of Explosive Ordnances (EOD),



Removal of duds...



Demining...



Terroristic attacks...

... require human interventions in military and civil areas

- Operations are
 - + hazardous
 - + delicate
 - + complex
 - + expensive



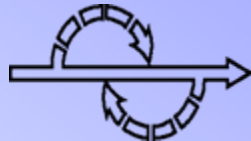
- Experts **act manually** close to the explosive object

➔ Demand for assistance by remote control



Outline

- **State-of-the-art remote EOD**
- Telepresent control
- Bimanual haptic telepresence system
 - hardware setup
 - control architecture
 - safety features
- Experimental results from typical EOD scenario



State-of-the-art Technology for Remote EOD



system example: Revolution, REMOTEC, UK

- mobile platform
- single-arm manipulator
- direct visibility
- simple control panel
- radio communication

Major deficiencies:

- simple actions only
- visual feedback only
- non-intuitive operation
- confined feeling of presence

➔ Complex actions at the explosive still need manual intervention



Outline

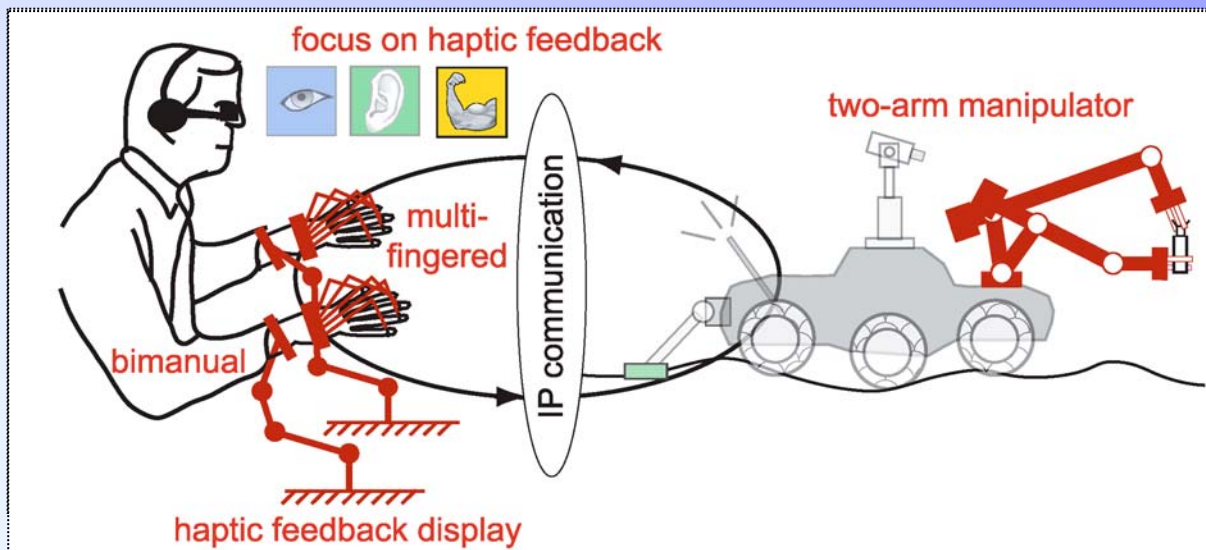
- State-of-the-art remote EOD
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Advanced Remote EOD . . .

. . . should provide an increased sensation of operator immersiveness via

- multimodal perceptual feedback,
e.g. haptics = **touch** and **force**, stereo vision
- two-arm manipulator system
- intuitive human system interface (HSI)

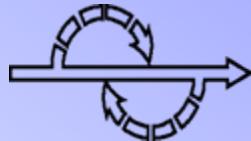
➔ Apply **haptic telepresence control technology** to EOD



Two-arm manipulator
and stereo vision
on mobile platform

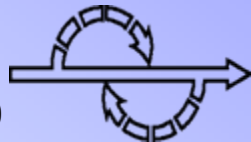
*What I hear I forget,
what I see I remember,
what I **touch** I understand.*

Confucius 551 – 479 BC



Outline

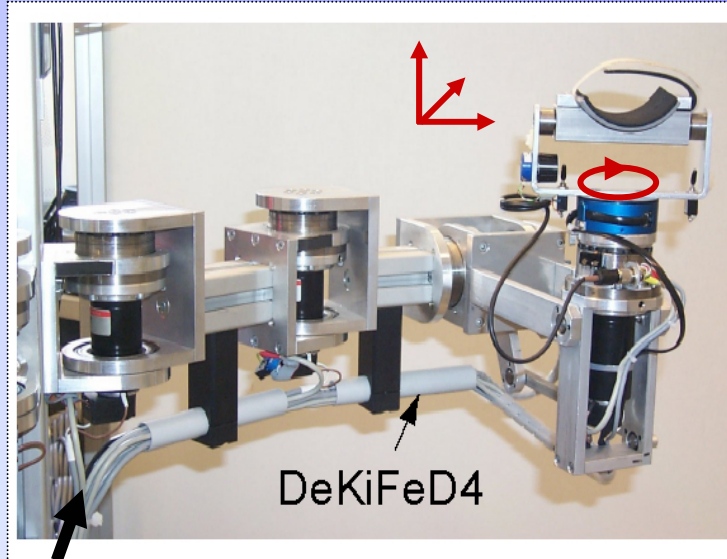
- ✓ State-of-the-art remote EOD
- ✓ Telepresent control
- **Novel bimanual haptic telepresence system**
 - **Hardware Setup**
 - bilateral control architecture
 - safety features
- Experimental results from typical EOD scenario



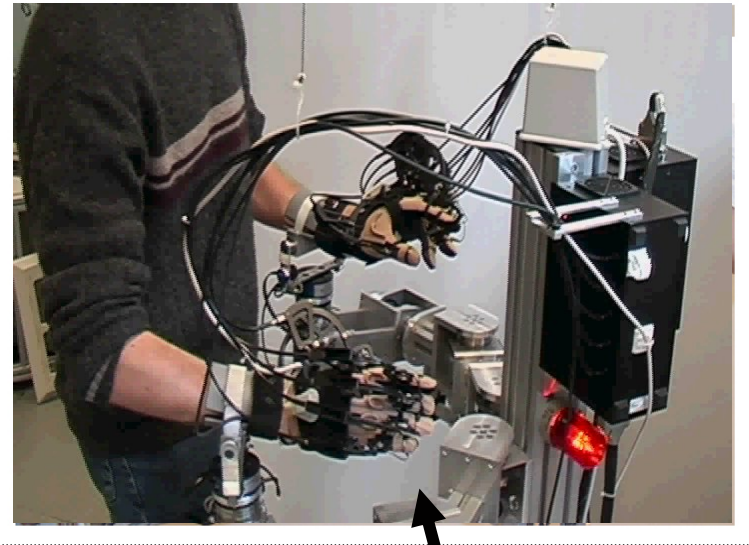
Haptic Feedback Display

Parallel wrist and finger force feedback display:

(ii) Finger kinesthetic display



(i) Powerful desktop kinesthetic feedback device

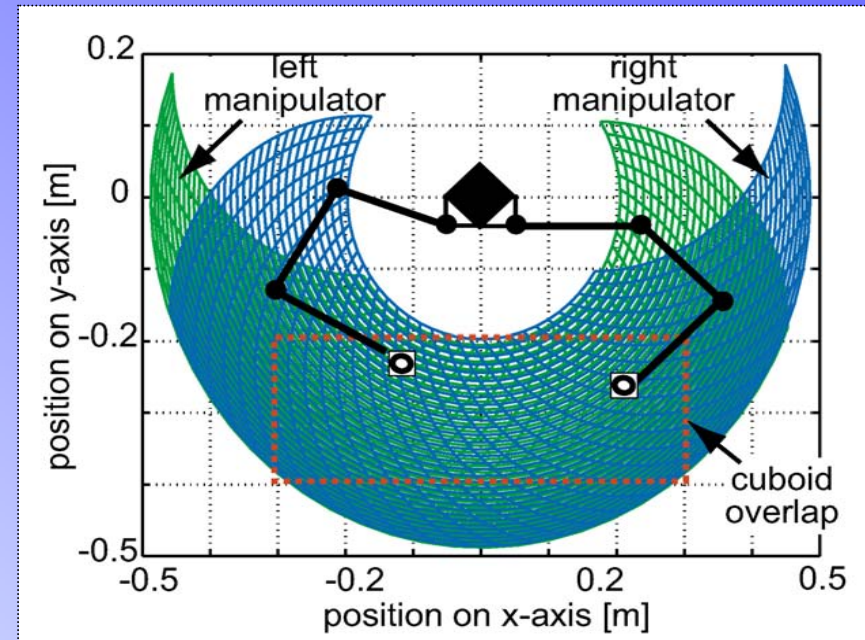
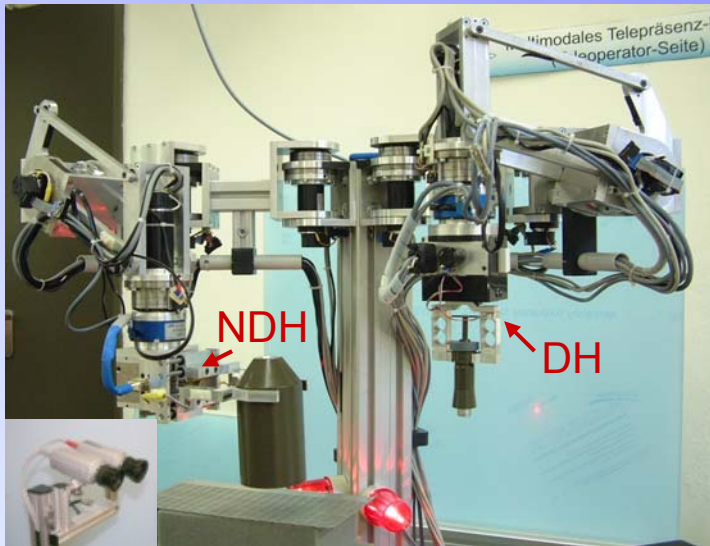


(iii) Bimanual display with mirrored joint configuration

- SCARA type, 4 active Cartesian DoFs (3 translations, 1 rotation)
- DC motors with Harmonic Drives
- wrist forces/torques: 120 N, 20 Nm; finger forces: 10 N
- force/torque sensor



Two-arm Manipulator



Gripper configuration

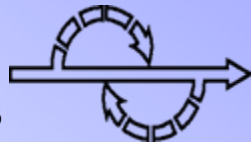
- non-dominant hand (NDH): stable grasp, horizontally arranged jaws
- dominant hand (DH): precise action, vertically arranged jaws

Workspace

- large overlap (60x20x30 cm³)

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Control Architecture for Wrist Kinesthetic Subsystem

requiring local control algorithms for master (display) and slave (manipulator)

Objectives:

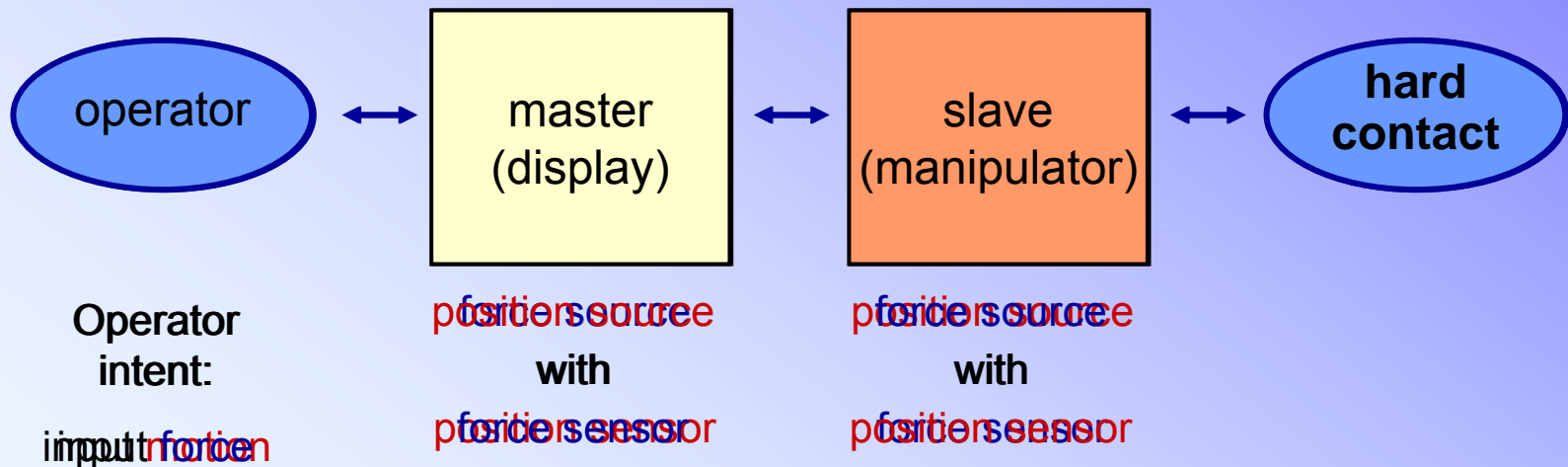
- robust stability
- realistic force feedback (= transparency)

Assumptions:

- communication delay $< 5\text{ms}$
- force, velocity data available

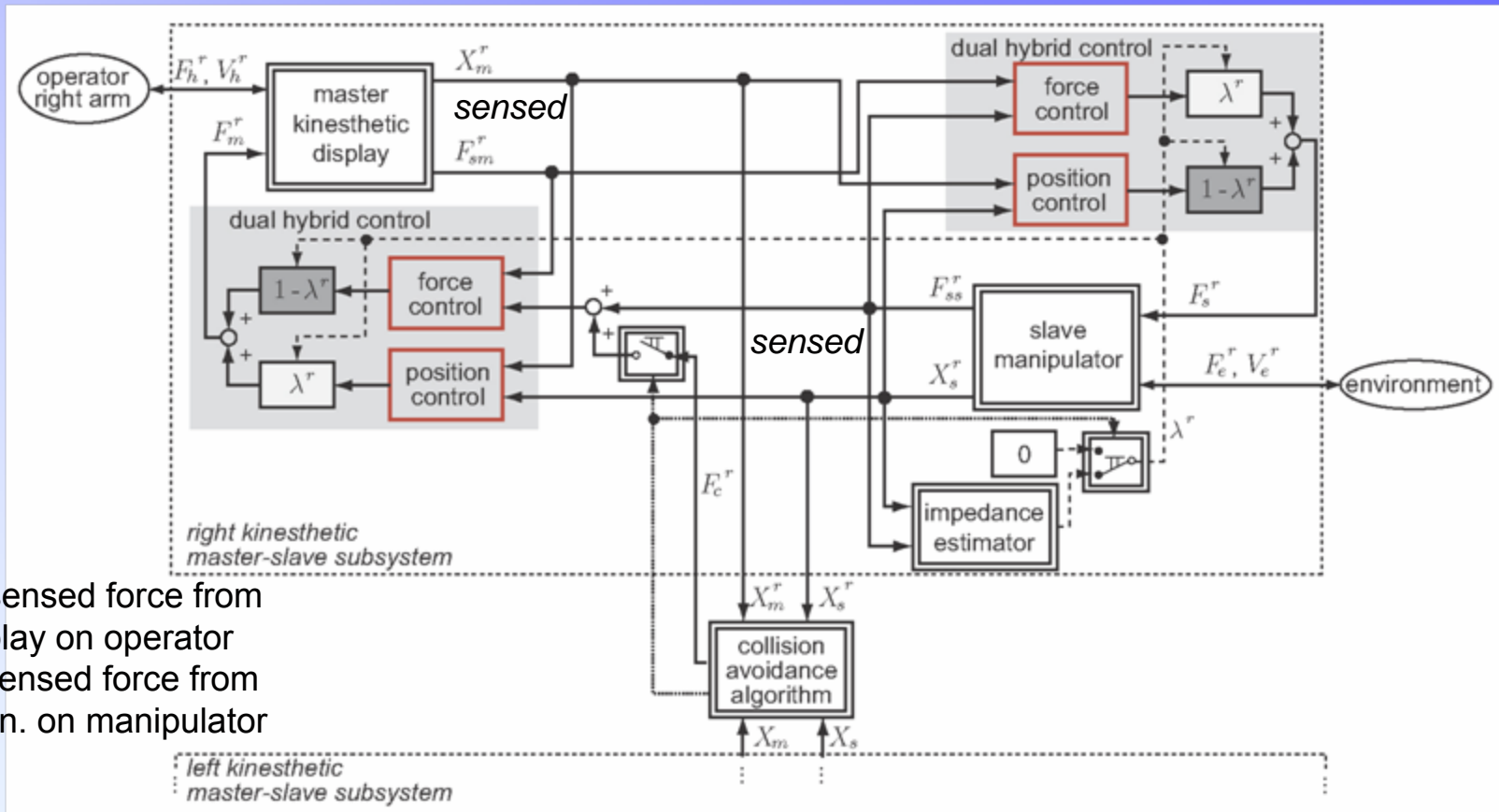
✗ Fixed control law for free motion or hard contact **not** appropriate

New paradigm: concept of dual-hybrid teleoperation [Reboulet, 1995]



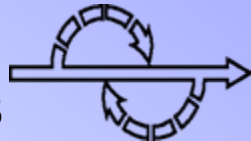
➔ Changing contact requires adaptation of control laws

Bi-manual Kinesthetic Control Architecture

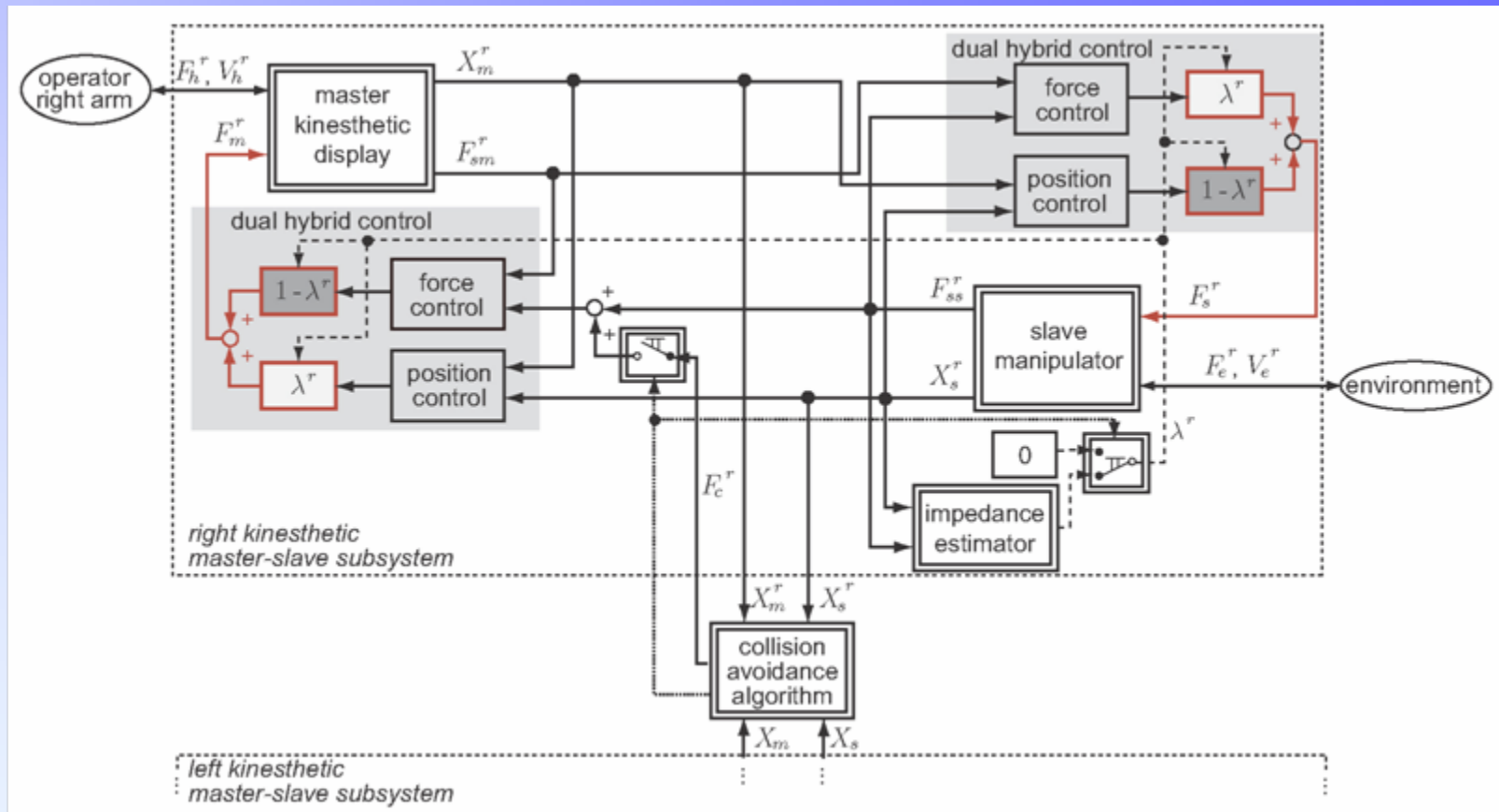


- F_{sm}^r : sensed force from display on operator
- F_{ss}^r : sensed force from environ. on manipulator

- sensor-based **force** controller
- state space **position** controller



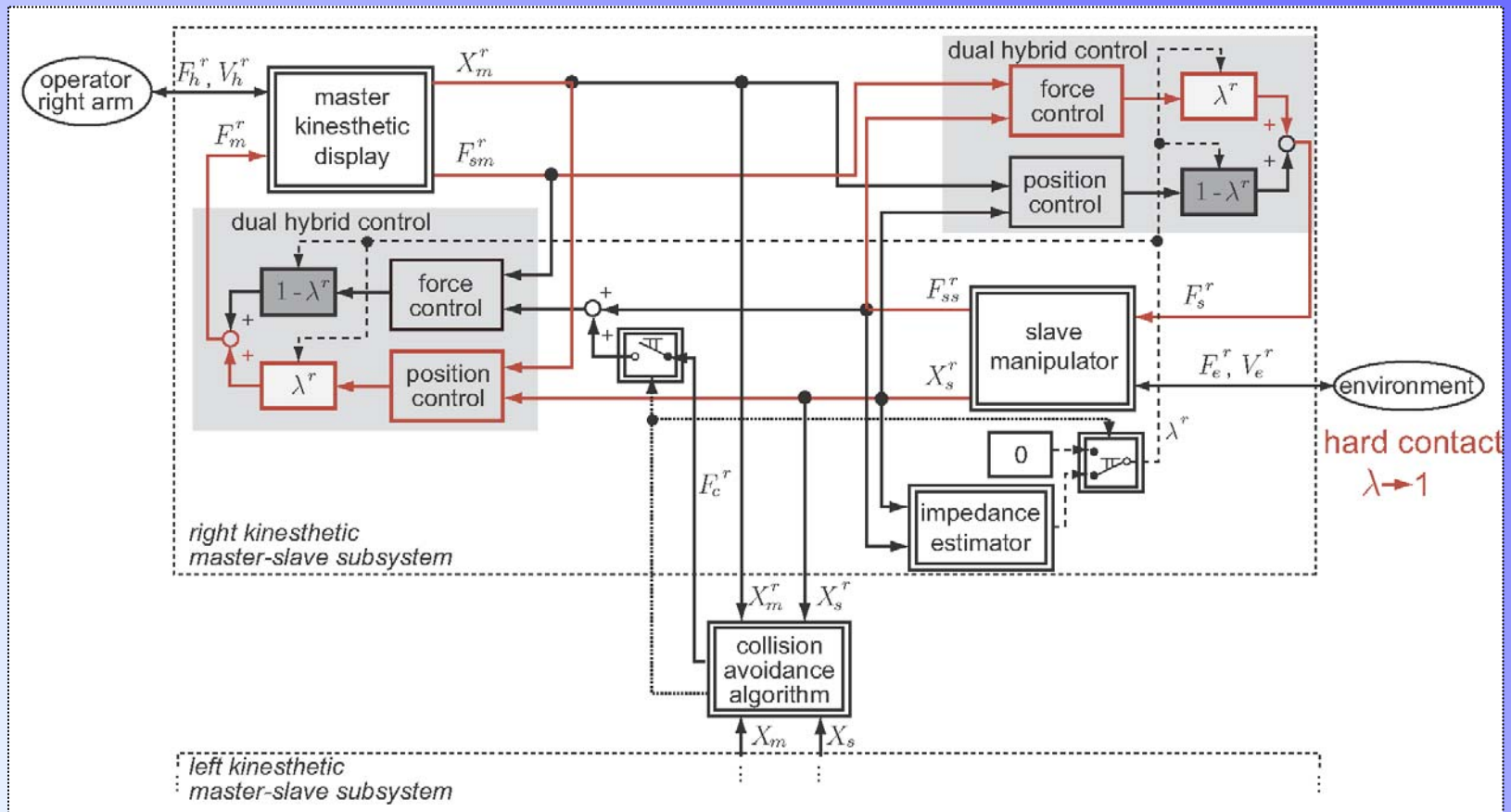
Bi-manual Kinesthetic Control Architecture



- summation of controller outputs weighted by $0 < \lambda < 1$
- duality of weighting λ on master and slave site



Adaptation of Control Laws

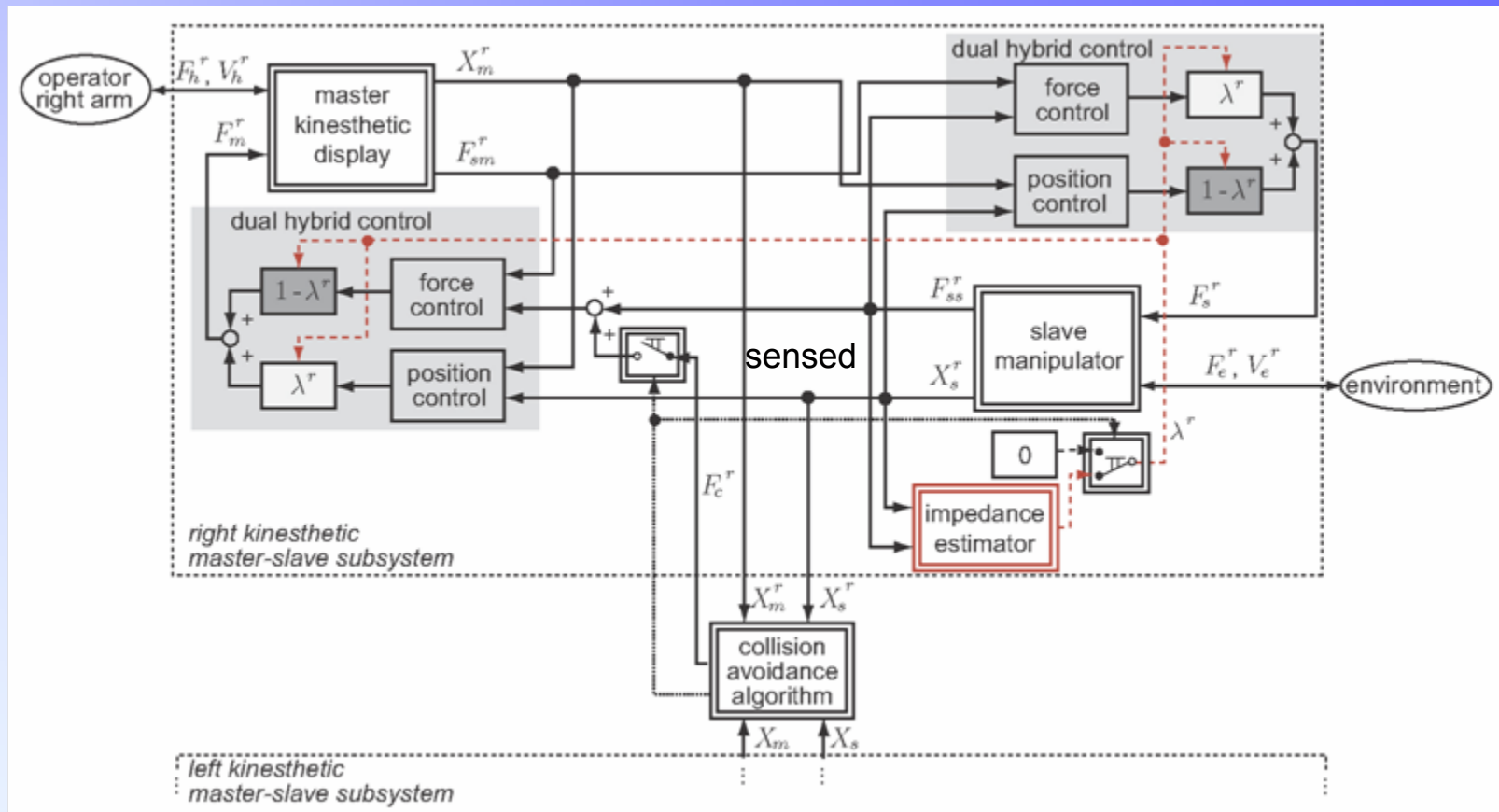


• free motion: $\lambda \approx 0$

• hard contact : $\lambda \approx 1$

➔ Adaptation assures stability and realistic environmental feedback (transparency)

Environmental Impedance Estimation



- on-line estimation using manipulator force/position data
- impedance model and recursive least square algorithm
- weighting factor $\lambda \rightarrow$ normalized impedance



Impedance Estimator

- Identification of 1st order impedance model

$$\hat{Z}_e = \hat{b}_e + \hat{k}_e/s$$

by recursive least square algorithm

Input: slave position and velocity

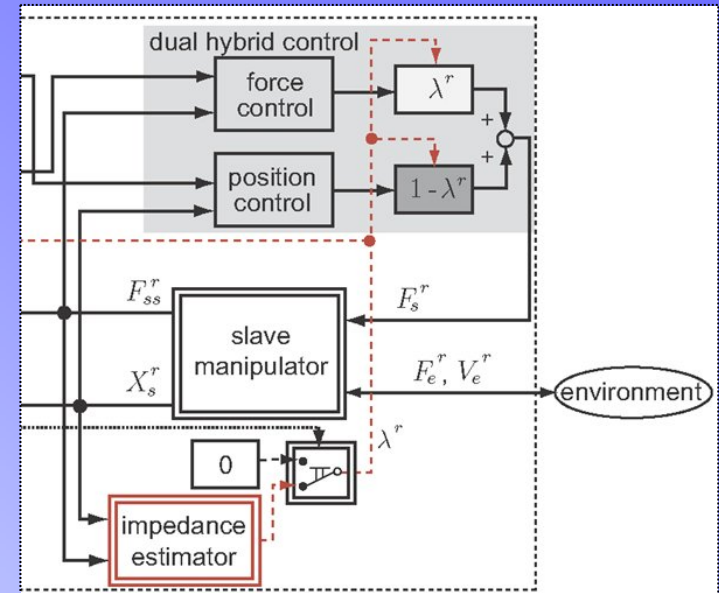
Output: slave force

- *Virtual impedance* measure with fixed frequency $\omega_u = 20$ rad/s

$$\tilde{Z}_e = |\hat{Z}_e|_{\omega=\omega_u} = \sqrt{\hat{b}_e^2 + \frac{\hat{k}_e^2}{\omega_u^2}}$$

- Preceding tests for identification of $\tilde{Z}_{e,max}$
- Normalized weighting factor defined as

$$\lambda = \tilde{Z}_e / \tilde{Z}_{e,max} \in [0, 1]$$

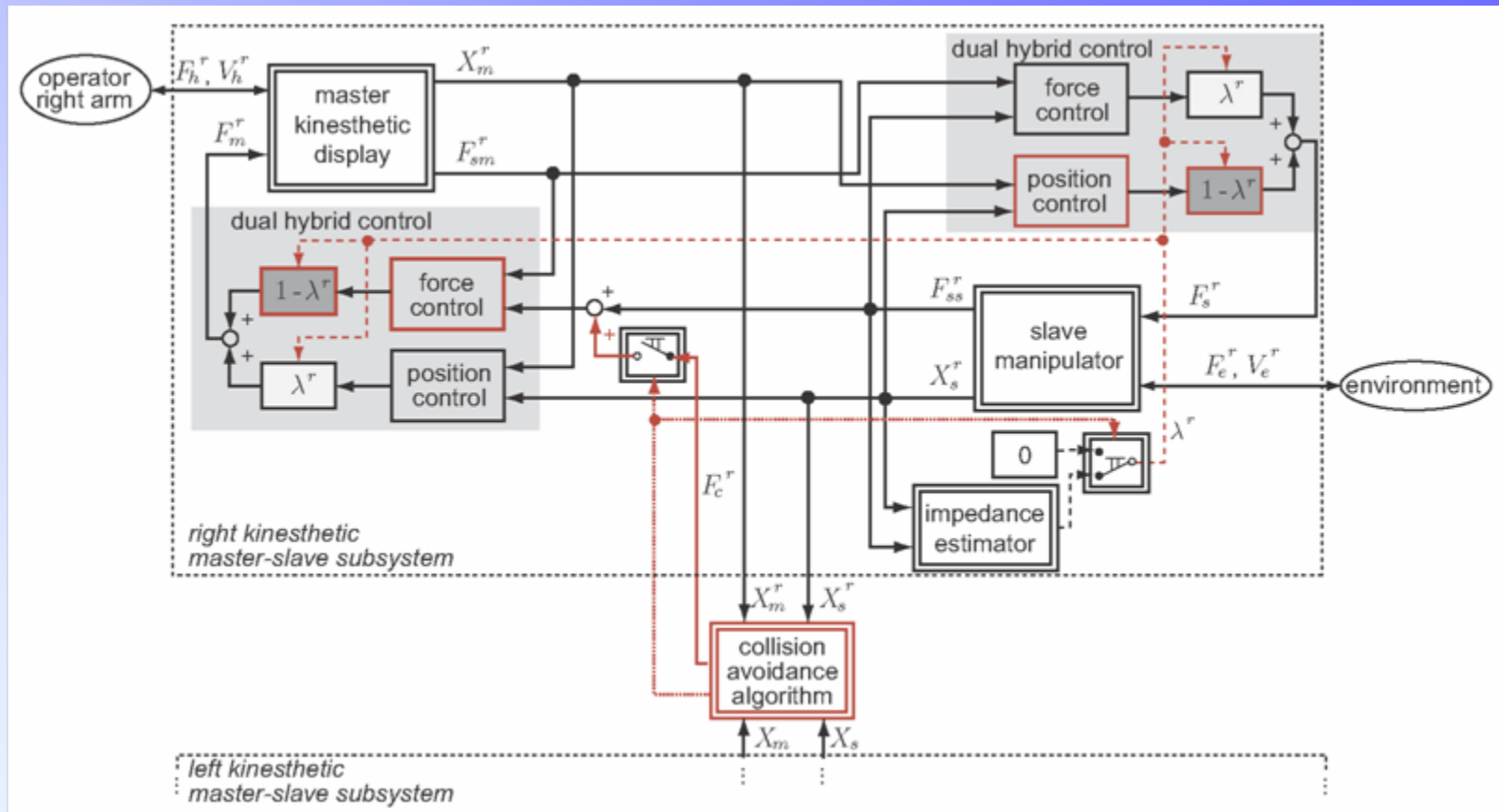


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Collision Avoidance, cont'd



- collision avoidance measures **override** mode adaptation:
 ➔ force controlled master & position controlled slave

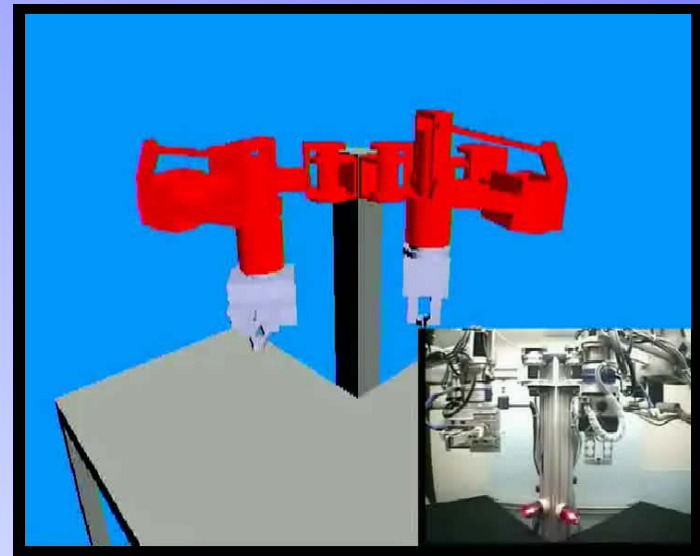
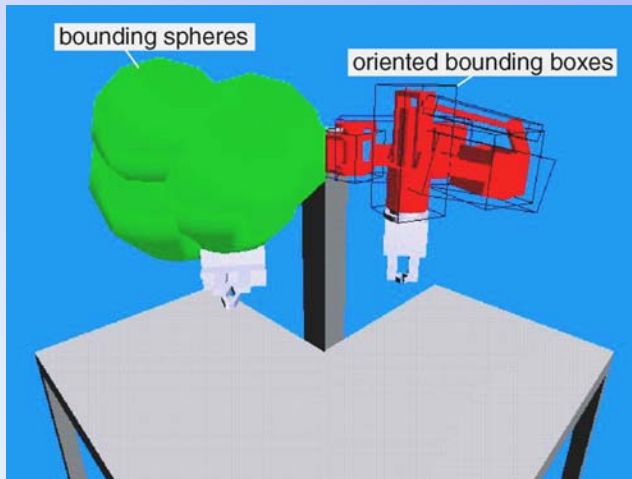


Active Manipulator Collision Avoidance

Requirements:

- collision prediction
- active collision avoidance
- ➔ **Augmented force feedback & virtual force arrows** in video images

Prediction algorithms: model-based

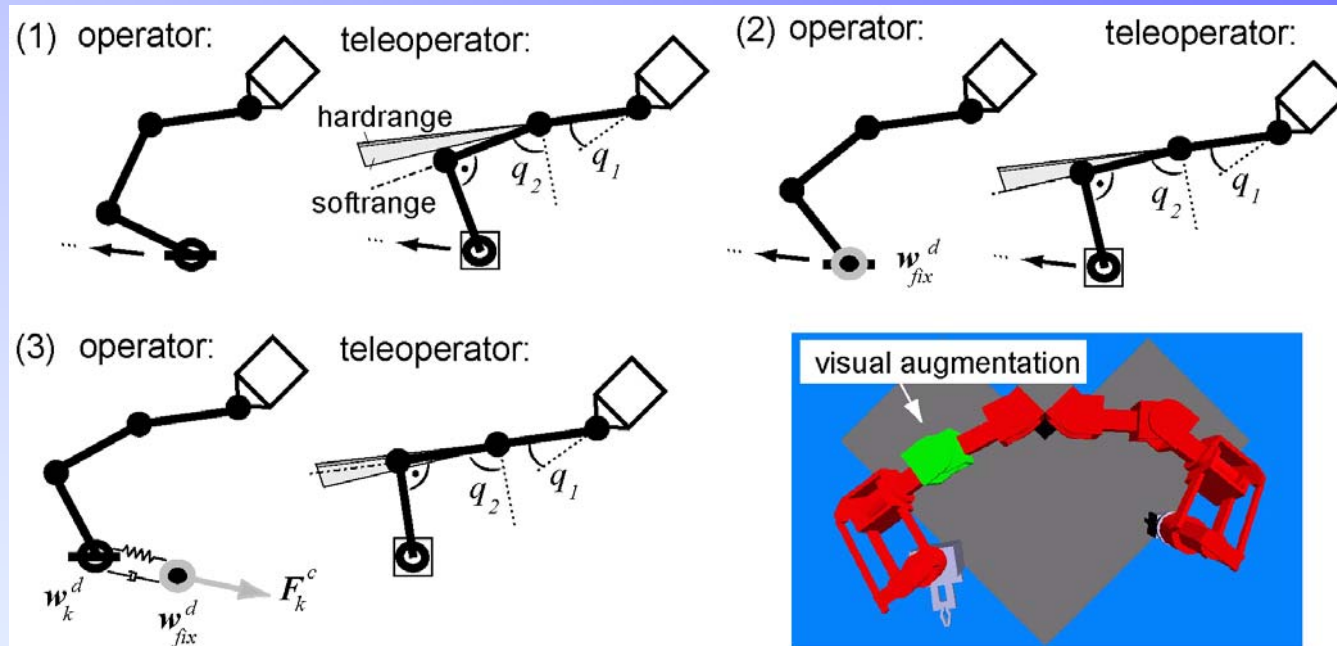


Computation of augmented forces:

- employing virtual spring-damper systems

Manipulator Workspace Penetration Avoidance

Workspace penetration by visual and haptic augmentation



- force computation:

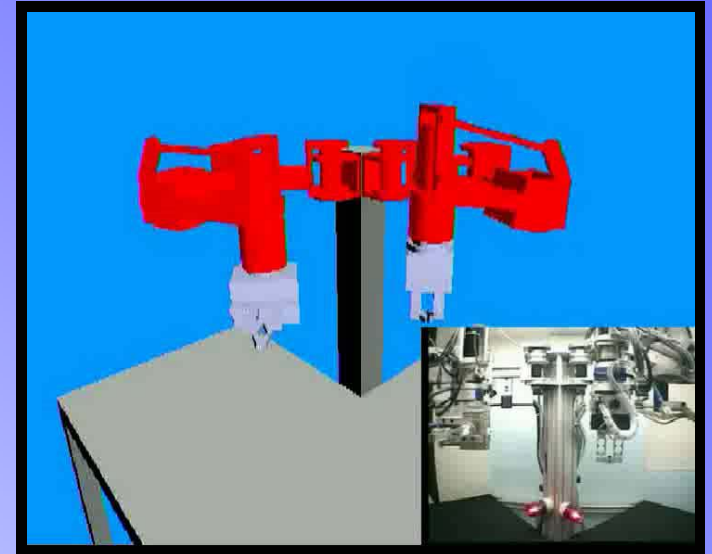
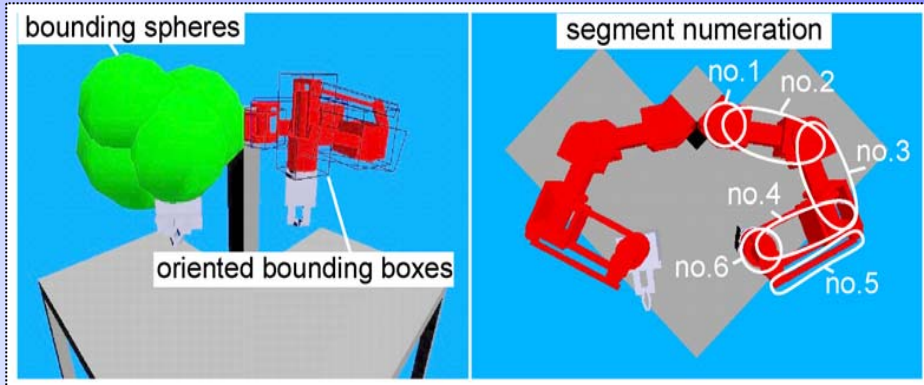
$$\mathbf{d}_k = \mathbf{w}_k^d - \mathbf{w}_{fix}^d$$

$$\mathbf{F}_k = \begin{cases} c_f \mathbf{d}_k + c_d \frac{\mathbf{d}_k - \mathbf{d}_{k-1}}{T_0} & |\mathbf{d}_k| > |\mathbf{d}_{k-1}| \\ c_f \mathbf{d}_k & |\mathbf{d}_k| \leq |\mathbf{d}_{k-1}| \end{cases}$$

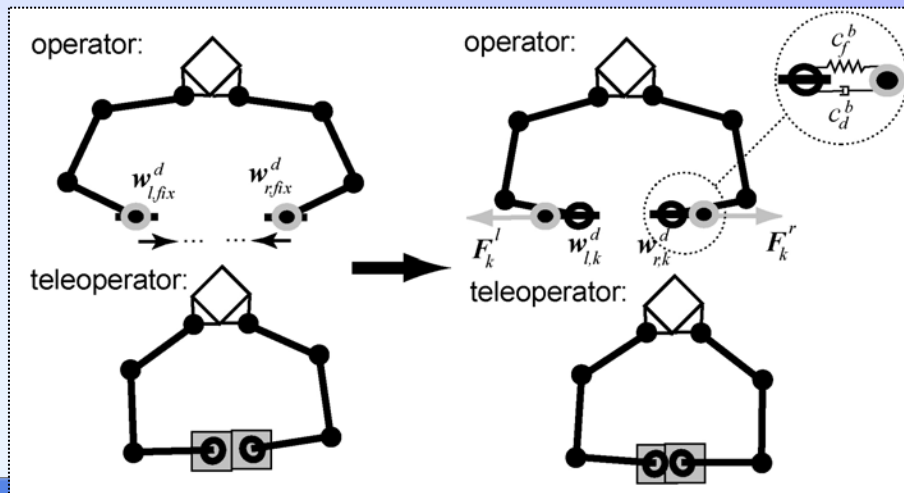
- if hard-range reached, all telemanipulator joints are fixed!

Active Manipulator Collision Avoidance

Collision prediction



Collision prevention by force feedback



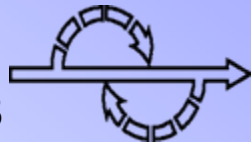
- force computation:

$$d_k = w_k^d - w_{fix}^d$$

$$F_k = \begin{cases} c_f d_k + c_d \frac{d_k - d_{k-1}}{T_0} & |d_k| > |d_{k-1}| \\ c_f d_k & |d_k| \leq |d_{k-1}| \end{cases}$$

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Evaluation in Cooperation with Experts from German Armed Forces

Manual demining operation



Telepresent Disposal of Fragmentation Mine

Operation in **remote** environment

**gripping mine
and
retaining element**



Some Experimental Findings

- demining task executed by 20 experts

Type of task execution	Time
manual (deminer's training)	60 s
remote demining:	
■ novice operator	800 s
■ trained expert	< 400 s

- efficient (7 : 1) and realistic support by HTP system
- activation of limbs experienced as being “natural”

Verbal statements from experts involved in evaluation:

- „ use of **both hands** for remote demining is highly useful “
- „ force feedback provides **reliable impression** of direct operation at the mine “
- „ parallel **force feedback at finger and wrist** is experienced as a consistent overall force perception “



Activation of Limbs ?

- 20 subjects operated manually, 20 other teleoperated
- subjects express perceived limb activations by percentages

SUBJECT'S DISTRIBUTED FORCE PERCEPTION AT THE LIMBS

contact forces		<i>manually</i>		<i>teleoperated</i>		grasp forces		<i>manually</i>		<i>teleoperated</i>	
distribution [%] at		\bar{x}	σ_x	\bar{x}	σ_x	distribution [%] at		\bar{x}	σ_x	\bar{x}	σ_x
shoulder		24.3	19.3	18.3	19.6	fingertip		46.8	15.0	47.5	21.7
elbow		21.3	16.1	21.3	16.3	phalanx		31.5	16.1	36.0	14.6
wrist		23.8	15.8	25.8	13.4	palm		8.5	8.8	6.9	8.8
finger		30.8	17.6	34.8	19.5	wrist		13.3	12.5	9.6	8.1
χ^2 -test		0.54		(0.760)		χ^2 -test		0.49		(0.785)	

No statistical significant difference between manual and teleoperated task execution!

➔ Realistic force feedback !

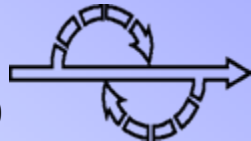


Conclusions

- EOD may benefit from adoption of available (bimanual haptic) telepresent control approaches
- Stability and transparency by structure adapting control architecture
- Active manipulator collision avoidance
- Encouraging results from evaluation with experts

Next steps

- Attach two-arm manipulator to **mobile platform**
- Extend maneuverability to **>4 DoF arm motions**
- Replace two-jaw grippers by **multi-fingered (≥ 3 fingers) hands**
- **Optimize** interconnection and device control algorithms for the case of **non-neglegible communication delays**



The End

